



Thermodynamic Analysis of a 500MWe Coal-fired Supercritical Power Plant with CO₂ Capture Integrated with Kalina Cycle for Combined Cooling and Power

Nitesh Kumar Choudhary^a, GoutamKhankari^b, SujitKarmakar^{a,*}

^aDepartment of Mechanical Engineering, NIT Durgapur, Durgapur-713209, India

^bMejia Thermal Power Station, Damodar Valley Corporation, West Bengal-722183, India

*E-mail: sujitkarmakar@yahoo.com

Manuscript Received online 6/16/2020, Accepted 8/11/2020

A thermodynamic study is carried out on a 500MWe coal based supercritical thermal power plant (base plant) with MonoEthanolAmine (MEA) based CO₂ capture unit integrated with a Kalina Cycle (Low-grade energy cycle) setup for Combined Cooling and Power (CCP) generation using Indian High Ash (HA) coal as fuel, and the results are compared with an imported Low Ash (LA) coal. The modelling and simulation of the different plant configurations are done by using the simulation software "Cycle-Tempo". The base plant is integrated with the CO₂capture unit working on MEA based post combustion carbon capture technique. The separated CO₂ is compressed to a pressure and temperature of 110 bar & 35°C, respectively for ease of transportation and storage. During the four-stage CO₂ compression the heat wasted through the intercoolers is utilized by using Kalina Cycle System. In Kalina cycle binary mixture of ammonia-water (NH₃-H₂O) is used as a working fluid. This mixture passes through the intercoolers of the CO₂ compression system and got vaporized by utilizing the waste heat. Thereafter, the vapour passes through the two-stage turbines with reheater resulting in additional power generation. The mixture is throttled after the condenser produces the cooling effect. There is about 1.72% of energy efficiency improvement of the proposed integrated plant in comparison with the base plant with CO₂ capture. There is about 1.7MW of additional electricity generation along with 5.7 MW of cooling effect (equivalent to 1632 TR) are obtained by this novel technique.

Keywords: Supercritical power plant, Kalina cycle, CO₂ Capture, Combined Cooling and Power (CCP)

Introduction

Fossil fuels are the dominant sources of energy which include coal, petroleum, natural gas etc. Coal is the largest abundant source of energy on the planet, but it generates lots of greenhouse gases. It has been projected that around 3084 million tonnes of CO₂ emission rise in India will take place by 2030, out of which 43% of CO₂ will be emitted from the pulverized coal-based power plants¹.

Moreover, the study says that the emission of CO₂ from all the existing coal fleet across the world would emit a cumulative 175 Giga tonnes of CO₂ by 2040 equivalent to 5 times of the total energy sector emissions in 2018². Such a huge amount of CO₂emission will deteriorate our environment; hence there is a dire need for novel technologies to limit or avoid the CO₂ emissions. The widely used techniques for the capturing of CO₂ are pre-combustion carbon capture, post-combustion



carbon capture and oxy-fuel combustion capture. CO₂ capturing through pre combustion technique is done prior to the combustion of fuel and hence, it is a less energy intensive process as compared to post combustion techniques. In post combustion process the CO₂ which is captured after combustion of fuel is done by physical or chemical adsorption or absorption processes and also by using membranes. In oxy-fuel combustion carbon capture technique, oxygen is supplied in the combustor resulting in high concentrated CO₂ emission, hence capture of CO₂ becomes easy. But this process is not economically feasible because lots of energy is required to produce O₂ through Air Separation Unit (ASU)^{3, 4}. Comparative studies show that Monoethanolamine (MEA) based chemical absorption process is the most economical and popular CO₂ capture technique due to high CO₂ capturing efficiency⁵. The CO₂ capture drops the plant efficiency significantly. The process heat available from CO₂ capture unit can be utilized for running low grade cycles. Some of the low grade cycles are Kalina Cycle, Organic Rankine Cycle (ORC), CO₂ transcritical power cycle etc. out of which ORC system is one of the suitable cycles for waste heat recovery at low temperature because each process is optimal at different operating ranges of the cycle. But due to low temperature range the overall efficiency of this cycle is poor⁶. In contrast, Kalina cycle plays an important role for waste heat recovery because it is very efficient technology for low grade waste heat power generation⁷. Zhang et al. are carried out an analysis based on energy and exergy of a cogeneration plant between ORC and absorption heat pump, where waste heat are recovered from the exhaust of the steam turbine and the result shows that there is an

increase in energy efficiency by 9.38% and 1.71% of exergy efficiency⁸. Campos et al. have done the thermo-economic optimization on the ORC, and the cycle is used to recover the waste heat of flue gas from the micro gas turbine and the result shows an additional electrical power generation of 14.1kW⁹. Özahi et al. are carried out an optimization on Kalina cycle added with a municipal solid waste based power plant running based on the waste heat from the exhaust gas and the result shows that there is an improvement in efficiency of 3.62%¹⁰. Abamet al. did the thermodynamic and economic analyses of a Kalina cycle integrated with an absorption refrigeration system for Combined Cooling and Power (CCP) production resulting in 1077kW of cooling effect¹¹.

Advantages of using a Kalina cycle instead of ORC is that it uses a mixture of ammonia and water which possess variable boiling temperatures. Another major advantage being lesser irreversibilities associated during heat transfer process. It also has a lower Ozone Depletion Potential (ODP) and has efficient thermo-physical properties¹². Due to its higher efficiency, Kalina cycle is chosen for utilizing the waste heat coming from the intercoolers of the CO₂ capture unit.

In the present study, a thermodynamic analysis is carried out for a 500MW_e supercritical power plant with Kalina Cycle integrated CO₂ capture unit for CCP. MEA based post combustion CO₂ capture technique is used for capturing CO₂. After the extraction of CO₂, it is compressed to reach into the supercritical state for ease of transportation and storage. During the compression process, there is a rise in temperature in the intercoolers used in the CO₂ compression system, The waste heat generated from the intercoolers is utilized in



Kalina Cycle for additional power generation and getting the cooling effect.

Plant Configurations

In our present work, a 500MW_e supercritical power plant (Base plant) is considered as a standalone plant with steam parameters of 242.2 bar/537°C/565°C. It has one stage reheating process¹³ and after reheating, the final temperature of feed water is about 280°C. The plant having several types of turbine and feed water heaters which are one high pressure (HP) turbine, one intermediate pressure (IP) turbine and two low pressure (LP) turbine, three HP feed water heaters and four LP feed water heaters. This base plant is integrated with CO₂ capture unit, in the CO₂ capture unit the flue gas from the air pre-heater is passed through the moisture separator wherein moisture is separated by condensation. Then the flue gas is passed through the CO₂

separator, where flue gas and solvent (MEA) flow in opposite direction. During this process, CO₂ gets absorbed by the solvent. The rich MEA is passed through the reboiler where the absorbed CO₂ is separated out; the energy required for the regeneration is provided by the steam. The required steam is bled from the line between IP turbine and LP turbine and from the reboiler the steam is again feedback to the LP feed water heater. Since huge amount heat is being extracted so it reduces the efficiencies. After the separation, the CO₂ is compressed to a particular pressure and temperature (110 bar & 35°C) to reach into supercritical state¹⁴, for which four stage intercooler is required to compressed the CO₂ at that point. The schematic of base plant added with CO₂ capture unit is shown in fig.1.

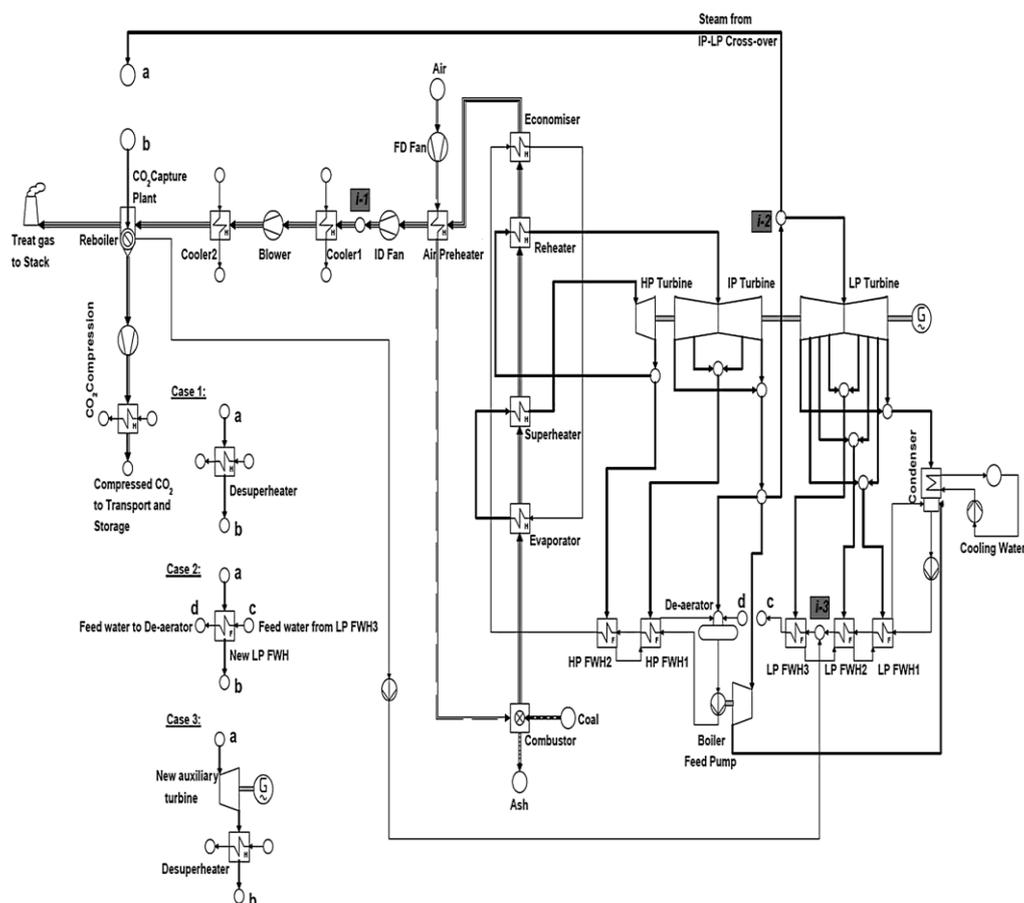


Fig.1. Base Plant with CO₂ capture unit¹⁴.

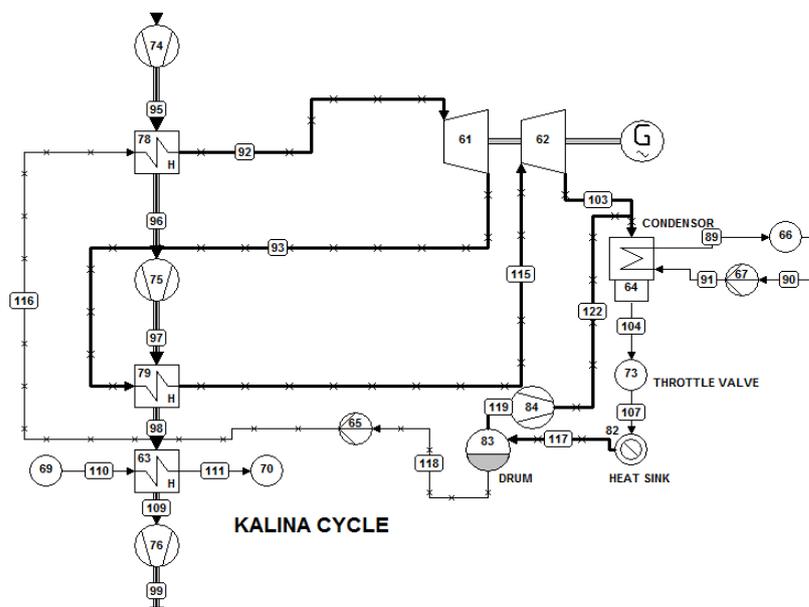


Fig. 2. Kalina cycle integrated with CO₂ capture unit.



In the proposed plant configuration, Kalina cycle is integrated with CO₂ capture unit of the plant for utilizing the waste heat, which is being available at intercooler of CO₂ compression process. After the expansion process from two stage turbines in the Kalina cycle, the working fluid goes through the condenser after that one throttle valve is added for decreasing the temperature and the lower temperature working fluid then passes through the heat sink where heat extraction will take place from the coolant space. Then, the working fluid passes through the drum where the separation of liquid and gaseous form takes place. The liquid form of working fluid is sent back to the intercooler of CO₂ compression process. After the absorption of heat, it is converted into vapor form and sent to the turbine and the process continues. The schematic of Kalina system integrated with the intercooler of CO₂ capture unit is shown in fig.2.

Methodologies

Thermodynamic analysis of the proposed model is performed using commercially available software called 'CYCLE-TEMPO'¹⁵. The software performs the mass, species, energy and exergy balance across all the components of the plant using the following governing equations:

- Mass Balance:

$$\sum_i \dot{m}_i = \sum_o \dot{m}_o$$

- Energy Balance:

$$\sum_i \dot{m}_i h_i + \dot{Q}_{cv} = \sum_o \dot{m}_o h_o + W_{cv}$$

- Exergy Balance:

$$\sum_i \dot{m}_i \Psi_i + \dot{X}_{heat} = \sum_o \dot{m}_o \Psi_o + \dot{W}_{cv} + \dot{I}$$

- Chemical Species Balance:

$$\sum_o \dot{N}_j = \sum_i \dot{N}_j + \dot{N}_p$$

The various components of the plant are drawn and connected using appropriate chosen streams available from the components/fuel stream library available in the software.

The component modelling starts with process flow diagram of the power plant followed by specifying different operating conditions for all individual components like pressure, temperature, flow rate at inlet/outlet, efficiencies of compressor, pump, motor.

Fuel characteristics

The Indian coal considered as fuel is of high quality and low graded coal because of its low sulphur content and high mineral content. Hence, this coal is called as HA coal. Because of HA and low carbon content, Indian coal has a lower heating value. In this analysis the Higher Heating Value of HA coal and LA coal are estimated as 15.83 MJ/kg & 27.42MJ/kg based on as dry basis. The characteristics of coal are given in Table 1.

Table 1.Coal characteristics¹³

| | Indian high ash coal Dry (wt%) | Imported low ash coal Dry (wt%) |
|-----------------------|-----------------------------------|------------------------------------|
| Proximate analysis | | |
| Fixed carbon | 27.27 | 60.47 |
| Volatile matter | 23.96 | 22.85 |
| Ash | 48.87 | 16.68 |
| Ultimate analysis | | |
| Carbon | 39.16 | 69.8 |
| Hydrogen | 2.76 | 3.58 |
| Oxygen(by difference) | 7.92 | 7.66 |
| Nitrogen | 0.78 | 1.73 |
| Sulphur | 0.51 | 0.55 |
| Ash | 48.87 | 16.68 |



Performance parameters

There are following parameters based upon that the calculation part has done:

- Energy Efficiency (η) of the plant

$$= \frac{\text{Net power output of the plant}}{\text{Mass flow rate of the coal} \times \text{Higher heating value of coal}}$$

- Exergy Efficiency (ϵ) of the plant

$$= \frac{\text{Net power output of the plant}}{\text{Mass flow rate of the coal} \times \text{specific exergy of coal}}$$

- Net Efficiency with CCP

$$= \frac{\text{Net power output} + \text{heat absorbed through the coolant space}}{\text{Mass flow rate of the coal} \times \text{Higher heating value of coal}}$$

Assumptions

Following assumptions are given below based upon that the thermodynamic analysis has done

- On the basis of Indian climatic condition the relative humidity, temperature and pressure are 60 %, 33°C and 1.013 bar, and the composition of air is (in mole %) Nitrogen=75.62, Oxygen=20.30, Water=3.12, Carbon dioxide=0.03, Sulphur dioxide=0.01, others=0.92
- 7.5% of total energy production is assumed to be the auxiliary power consumption of the Supercritical power plant.
- Recovery of CO₂ is 85% with 98% of CO₂ purity.
- The efficiency of the pumps is 85 %.
- Rich and weak ammonia-water mixtures are saturated at the exit of the separator.

Results and Discussion

There is a comparison of efficiencies between the base plant with CO₂ capture and the proposed model based on

HA and LA coal, that are presented on Table 2 and Table 3.

From the analysis, it has been seen that there is a significant difference in energy efficiency and exergy efficiency for LA coal as compared with HA coal.

Table 2. Efficiencies of the plant with CO₂ capture

| Plant Efficiency (%) | High ash coal | Low ash coal |
|----------------------|---------------|--------------|
| Energy Efficiency | 28.41 | 29.52 |
| Exergy Efficiency | 25.02 | 27.64 |

Table 3. Efficiencies of the proposed model

| Plant Efficiency (%) | High ash coal | Low ash coal |
|----------------------|---------------|--------------|
| Energy Efficiency | 28.90 | 30.09 |
| Exergy Efficiency | 25.10 | 27.80 |

It is observed that in the proposed model, by utilizing the waste heat there is some increment in efficiency compared with the existing power plant with CO₂ capture unit.

Energy balance of the proposed model:

The energy balance of the proposed model is given in Table 4. It tells about quantity-wise losses of different components. The losses are calculated by the ratio between the losses of energy through the component and the heat energy input from the coal. It shows that maximum heat rejection occurs at the condenser. In this power plant, there is an additional loss of energy in flue gas cooling before entering into the separation unit, which is near about



6.22% for HA coal and about 5.09% for LA coal. Some part of energy is utilised in the compression of CO₂.

Table 4. Energy balance of the proposed model

| Components (%) | High | Low |
|---|----------|----------|
| | ash coal | ash coal |
| Energy efficiency of plant | 27.81 | 29.24 |
| Condenser | 21.99 | 22.09 |
| Heat loss in steam cooling for MEA regeneration | 29.96 | 30.09 |
| Bottom ash | 0.84 | 0.70 |
| Heat rejected through stack | 2.92 | 3.75 |
| Combustor | 1.44 | 1.53 |
| Heat loss during flue gas cooling | 6.22 | 5.09 |
| Heat loss during intercooling in compressors | 3.18 | 3.21 |
| Heat loss in cooling water (Kalina cycle condenser) | 1.43 | 1.49 |
| Other losses (by difference) | 4.17 | 2.78 |

Exergy balance of the proposed model:

The exergy balance using two types of coal is shown in the Table 5. It tells about quality wise losses at a different component of the plant, and it reveals that in the combustor losses are very high because of the irreversibility during the heat transfer and combustion process. The maximum losses occur in the combustor. The exergy destructions in CO₂ compression is 5.40 % for HA coal and 5.76 % for LA coal

Parametric analysis of the proposed model:

A sensitivity analysis is done to study the impact of pressure on the energy efficiency of the plant and it is shown in Fig.3. It is found in Fig. 3 that work output from Kalina cycle shows an increasing trend

corresponding to the rise in inlet pressure of the first turbine.

Table 5. Exergy balance of proposed model

| Components (%) | High | Low |
|--|----------|----------|
| | ash coal | ash coal |
| Exergy Efficiency | 25.10 | 27.80 |
| Losses in combustor | 33.54 | 28.64 |
| Loss in steam generation (Excluding Combustor) | 17.7 | 19.22 |
| Turbines | 2.57 | 2.71 |
| Stack | 0.91 | 1.57 |
| Condenser and cooling water | 0.97 | 1.03 |
| Loss in steam cooling for MEA regeneration | 6.64 | 7.02 |
| Compressed CO ₂ stream | 5.37 | 5.76 |
| Heat exchangers | 1.54 | 1.63 |
| Compressors | 0.7 | 0.78 |
| Ash | 0.47 | 0.41 |
| Other losses (by difference) | 4.49 | 3.42 |

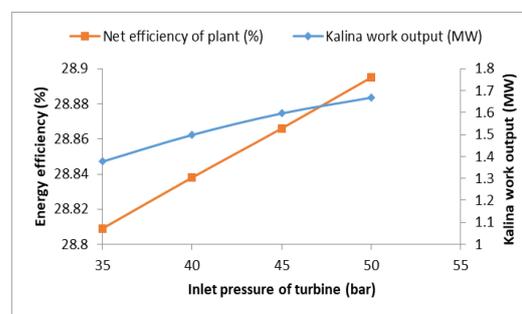


Fig. 3. Effect of inlet pressure on Kalina work output and Net efficiency of plant for HA coal.

A parametric study on the efficiency of the plant with the mass fraction of ammonia is also shown in Fig.4. It is observed that efficiency increases with an increase in ammonia mass fraction in the working fluid of Kalina cycle as higher ammonia fraction causes lower boiling temperature at fixed pressure that helps to



reduce irreversibility in the heat exchanger and produce more vapor mass flow rate.

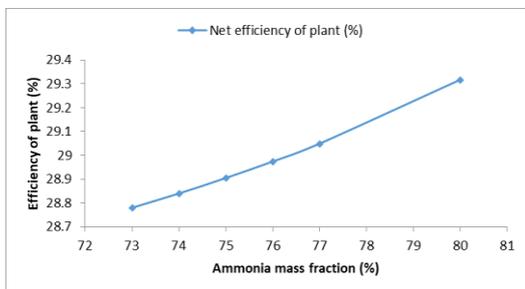


Fig. 4. Effect of mass fraction of ammonia on Net efficiency of plant for HA coal

Similarly, for LA coal feed power plant, sensitivity analysis on the energy efficiency of the plant is also studied. The work output from Kalina cycle shows an increasing trend corresponding to the rise in inlet pressure of the first turbine as shown in Fig.5, whereas the parametric study on efficiency of the plant with the ammonia mass fraction is shown in Fig.6. It is observed that efficiency increases with increase in ammonia mass fraction in the working fluid of Kalina cycle.

The Kalina cycle integrated CO₂ capture unit with the base plant helps in producing about 1.7MW of additional electricity along with 5.7 MW of cooling effect which is equivalent to 1632 ton of Refrigeration (TR).

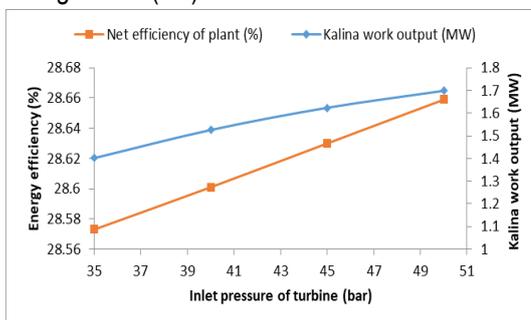


Fig. 5. Effect of pressure on Kalina work output and Net efficiency of plant for LA coal

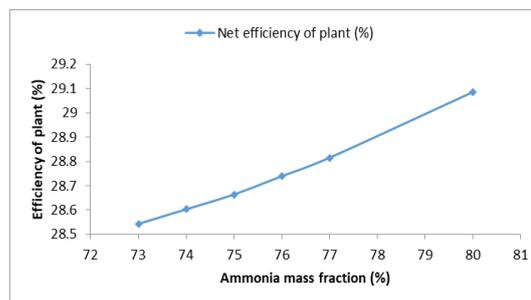


Fig.6. Effect of NH₃ mass fraction on Net efficiency of plant for LA coal

Additional Power Generation and Cooling effect:

Conclusions

From the thermodynamic analysis of the proposed model, the following major conclusions are drawn:

- 1) There is about 1.72 % increase in energy efficiency and 0.31% increase in exergy efficiency as compared to the existing power plant with CO₂ capture due to additional power output and cooling effect.
- 2) In energy balance, maximum losses occur in the condenser and also during MEA regeneration whereas, exergy balance shows maximum losses take place in the combustor.
- 3) By increasing pressure at the inlet of Kalina cycle turbine, the efficiency and power output can be increased.
- 4) With increasing ammonia mass fraction, the cycle efficiency can also increase.
- 5) This novel technique delivers about 1.7MW of additional electrical power and about 5.7 MW of cooling effect (equivalent to 1632 TR).

References

1. A. Garg and P. R. Shukla, Coal, energy security for India: Role of carbon dioxide (CO₂) capture and storage (CCS), 2009, 34(8), 1032-1041.



2. International energy agency (IEA), <https://www.iea.org/reports/the-role-of-ccus-in-low-carbon-power-systems/the-co2-emissions-challenge>, 2020.
3. H. Coninck, M. Loos, B. Metz, O. Davidson, and L. Meyer, IPCC special report on carbon dioxide capture and storage, Intergovernmental Panel on Climate Change, 2005.
4. A. B. Rao, and E. S. Rubin, A technical, economic, and environmental assessment of amine-based CO₂ capture technology for power plant greenhouse gas control, *Environmental science & technology*, 2002, 36(20), 4467-4475.
5. A. L. Kohl, and R. B. Nielsen, *Gas purification* 5th ed. Houston: Gulf Publishing Company, 1997.
6. X. Zhang, L. Wu, X. Wang, and G. Ju, Comparative study of waste heat steam SRC, ORC and S-ORC power generation systems in medium-low temperature, *Applied Thermal Engineering*, 2016, 106, 1427-1439.
7. A. I. Kalina, Combined cycle and waste heat recovery power systems based on a novel thermodynamic energy cycle utilizing low-temperature heat for power generation, In *Turbo Expo: Power for Land, Sea, and Air*, American Society of Mechanical Engineers, 1983, 79368, p. V001T02A003.
8. H. Zhang, Y. Liu, X. Liu, and C. Duan, Energy and exergy analysis of a new cogeneration system based on an organic Rankine cycle and absorption heat pump in the coal-fired power plant, 2020, 223, 113293.
9. G. B. de Campos, C. Bringhenti, A. Traverso, and J. T. Tomita, Thermo-economic optimization of organic Rankine bottoming cycles for micro gas turbines, 2020, 164, 114477.
10. E. Özahi, and A. Tozlu, Optimization of an adapted Kalina cycle to an actual municipal solid waste power plant by using NSGA-II method, 2020, 149, 1146-1156.
11. F. I. Abam, T. A. Briggs, O. E. Diemuodeke, E. B. Ekwe, K. N. Ujoatuonu, J. Isaac, and M. C. Ndukwu, Thermodynamic and economic analysis of a Kalina system with integrated lithium-bromide-absorption cycle for power and cooling production, 2020, 6, 1992-2005.
12. G. Khankari, and S. Karmakar, Power generation from coal mill rejection using Kalina cycle, *Journal of Energy Resources Technology*, 2016, 138(5).
13. M. V. J. J. Suresh, K. S. Reddy, and A. K. Kolar, 3-E analysis of advanced power plants based on high ash coal, *International Journal of Energy Research*, 2010, 34(8), 716-735.
14. S. Karmakar, and A. K. Kolar, Thermodynamic analysis of high-ash coal-fired power plant with carbon dioxide capture, *International journal of energy research*, 2013, 37(6), 522-534.
15. Cycle-Tempo Release 5.0.: Delft University of Technology. Available online: <http://www.tudelft.nl>, 2008.